

ELECTRIC CIRCUITS ECSE-2010

Lecture 25.1



LECTURE 20.1 AGENDA

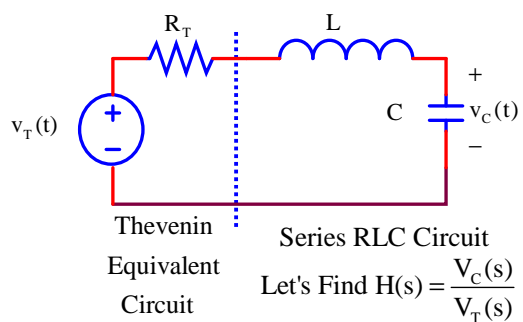
- Series Resonance

sawyes@rpi.edu

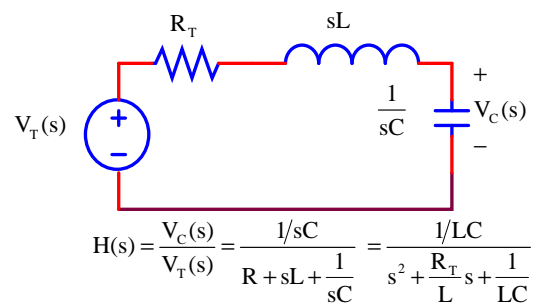
www.rpi.edu/~sawyes



SERIES RESONANCE



SERIES RESONANCE



SERIES RESONANCE

$$H(s) = \frac{V_C(s)}{V_T(s)} = \frac{1/LC}{s^2 + \frac{R_T}{L}s + \frac{1}{LC}}$$

$$= \frac{\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}$$

$$2\zeta\omega_0 = \frac{R_T}{L}, \quad \omega_0 = \sqrt{\frac{1}{LC}}$$

$$\zeta = \frac{R_T}{2} \sqrt{\frac{C}{L}}$$



SERIES RESONANCE

$$\zeta = \frac{R_T}{2} \sqrt{\frac{C}{L}}$$

For $\zeta < 1$, Circuit is Underdamped

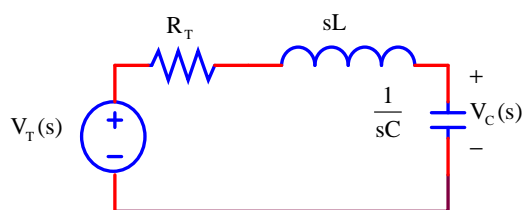
For Small R_T , Small C , Large $L \Rightarrow \zeta \ll 1$

Circuit is Very Underdamped

Let's Look at the Impedance of this Circuit



SERIES RESONANCE



$$Z(s) = R_T + sL + \frac{1}{sC}$$



SERIES RESONANCE

$$Z(s) = R_T + sL + \frac{1}{sC}$$

In AC Steady State:

$$Z(j\omega) = R_T + j\omega L - \frac{j}{\omega C}$$

$$= R_T + j(\omega L - \frac{1}{\omega C}) = R(\omega) + jX(\omega)$$

$$\text{At } \omega^2 = \frac{1}{LC} = \omega_0^2 \quad X(j\omega) \rightarrow 0$$



SERIES RESONANCE

$$Z(j\omega) = R_T + j(\omega L - \frac{j}{\omega C}) = R(\omega) + jX(\omega)$$

$$|Z(j\omega)| = \sqrt{R^2 + X^2}$$

$$X = \text{AC Reactance} \rightarrow 0 \text{ at } \omega = \omega_0 = \sqrt{\frac{1}{LC}}$$

ω_0 = Resonant Frequency

Series Resonant Circuit

$$|Z(j\omega_0)| = R_T = \text{Minimum at } \omega = \omega_0$$



SERIES RESONANCE

$$H(s) = \frac{V_C(s)}{V_T(s)} = \frac{\omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}; \quad \zeta = \frac{R_T}{2} \sqrt{\frac{C}{L}}$$

Let Input be a Sinusoid at $\omega = \omega_0; \Rightarrow s = j\omega_0$

$$H(j\omega_0) = \frac{\omega_0^2}{-\omega_0^2 + 2\zeta\omega_0(j\omega_0) + \omega_0^2} = \frac{\omega_0^2}{j2\zeta\omega_0^2}$$

$$|H(j\omega_0)| = \frac{1}{2\zeta} = \frac{2}{2R_T} \sqrt{\frac{L}{C}} = \frac{1}{R_T} \sqrt{\frac{L}{C}}$$



SERIES RESONANCE

$$|H(j\omega_0)| = \left| \frac{V_C(j\omega_0)}{V_T(j\omega_0)} \right| = \frac{1}{2\zeta} = \frac{1}{R_T} \sqrt{\frac{L}{C}}$$

$$\text{For Small } R_T, \text{ Small } C, \text{ Large } L \Rightarrow \zeta = \frac{R_T}{2} \sqrt{\frac{C}{L}} \ll 1$$

$$\text{For Small } R_T, \text{ Small } C, \text{ Large } L \Rightarrow \left| \frac{V_C}{V_T} \right|_{\omega=\omega_0} = \frac{1}{R_T} \sqrt{\frac{L}{C}} \gg 1$$

$$\text{For } \omega = \omega_0 \Rightarrow |V_C| \gg |V_T|$$

Series Resonance



SERIES RESONANCE

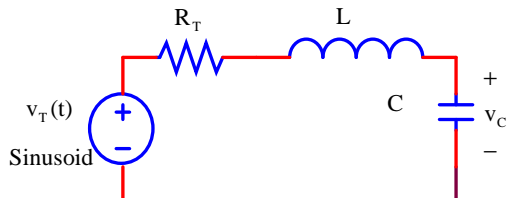
$$\text{For Small } R_T, \text{ Small } C, \text{ Large } L \Rightarrow \left| \frac{V_C}{V_T} \right|_{\omega=\omega_0} = \frac{1}{R_T} \sqrt{\frac{L}{C}} \gg 1$$

For $\omega = \omega_0 \Rightarrow \text{Output Voltage} \gg \text{Input Voltage}$

$$\text{For } \omega = \omega_0: \text{Voltage Gain} = \frac{|V_C|}{|V_T|} = Q_{\text{series}} = \frac{1}{2\zeta} = \frac{1}{R_T} \sqrt{\frac{L}{C}}$$



SERIES RESONANCE



$$R_T = 10 \, \Omega \text{ (small)}$$

$$L = 0.1 \text{ H (large)}$$

$$C = 1 \text{ nF (small)}$$

$$Q_{\text{series}} = \frac{1}{10} \sqrt{\frac{10^{-1}}{10^{-9}}} = 1000!!$$

$$|V_C| = 1000 |V_T| \text{ at } \omega = \omega_0$$



2ND ORDER FILTERS

General 2nd Order Bandpass Filter

$$H_{\text{BP}}(s) = \frac{Ks}{s^2 + 2\zeta\omega_0 s + \omega_0^2}; \text{ 1 Zero at Origin, 2 Poles}$$

General 2nd Order Notch Filter or Bandgap Filter

$$H_{\text{BG}}(s) = K \frac{s^2 + 2\beta s + \omega_0^2}{s^2 + 2\zeta\omega_0 s + \omega_0^2}; \text{ 2 Zeros, 2 Poles}$$



2ND ORDER FILTERS

- Let's Take a Closer Look at What Happens When We Have Real Poles, Repeated Poles and Complex Conjugate Poles for Low Pass, High Pass and Bandpass Filters
- All Will Exhibit Resonance if Poles are Complex Conjugates



2ND ORDER LOW PASS

$$\text{Low Pass: } H1_{\text{LP}}(s) = \frac{1000}{s^2 + 12s + 25}; \quad \zeta = 1.2$$

$$H2_{\text{LP}}(s) = \frac{1000}{s^2 + 10s + 25}; \quad \zeta = 1.0$$

$$\omega_0 = 5 \quad H3_{\text{LP}}(s) = \frac{1000}{s^2 + 8s + 25}; \quad \zeta = .8$$

$$H4_{\text{LP}}(s) = \frac{1000}{s^2 + .8s + 25}; \quad \zeta = .08$$

$$H5_{\text{LP}}(s) = \frac{1000}{s^2 + .08s + 25}; \quad \zeta = .008$$

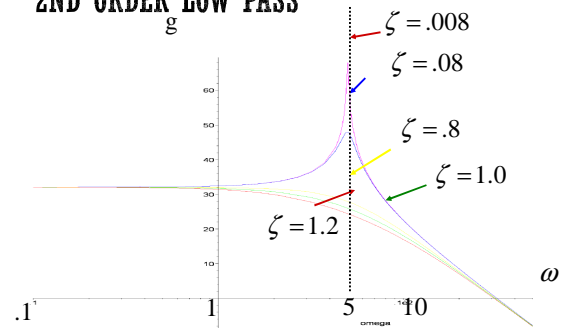


2ND ORDER LOW PASS

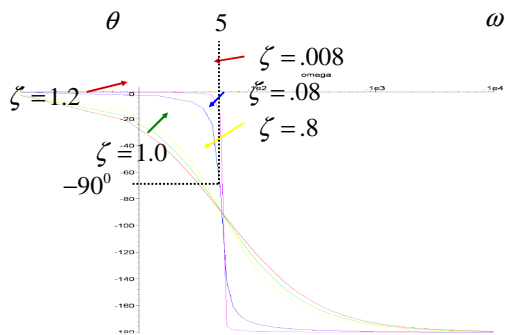
```
> with(plots):
Warning, the same changecoords has been redefined
> H1:=1000/(s^2+12*s+25):
> H2:=1000/(s^2+10*s+25):
> H3:=1000/(s^2+8*s+25):
> H4:=1000/(s^2+.8*s+25):
> H5:=1000/(s^2+.08*s+25):
> #Low Pass, wo = 5, Damping Ratio = 1.2, 1.0, .8, .08, .008
> #Overdamped, Critically Damped, Underdamped, Very Underdamped
> s:=I*omega:
> g1:=20*log10(abs(H1)):
> g2:=20*log10(abs(H2)):
> g3:=20*log10(abs(H3)):
> g4:=20*log10(abs(H4)):
> g5:=20*log10(abs(H5)):
> theta1:=(180/Pi)*argument(H1):
> theta2:=(180/Pi)*argument(H2):
> theta3:=(180/Pi)*argument(H3):
> theta4:=(180/Pi)*argument(H4):
> theta5:=(180/Pi)*argument(H5):
> semilogplot([g1,g2,g3,g4,g5],omega=1..50):
```



2ND ORDER LOW PASS



2ND ORDER LOW PASS



2ND ORDER HIGH PASS

High Pass: $H1_{HP}(s) = \frac{1000s^2}{s^2 + 12s + 25}; \zeta = 1.2$

$H2_{HP}(s) = \frac{1000s^2}{s^2 + 10s + 25}; \zeta = 1.0$

$\omega_0 = 5 \quad H3_{HP}(s) = \frac{1000s^2}{s^2 + 8s + 25}; \zeta = .8$

$H4_{HP}(s) = \frac{1000s^2}{s^2 + .8s + 25}; \zeta = .08$

$H5_{HP}(s) = \frac{1000s^2}{s^2 + .08s + 25}; \zeta = .008$

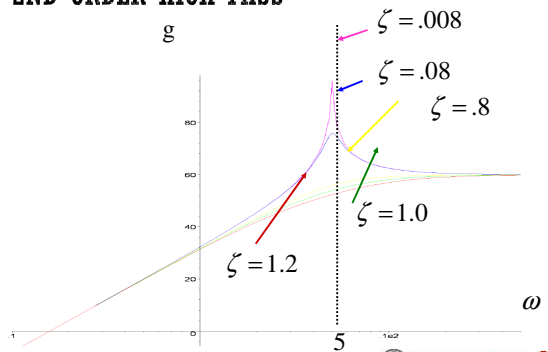


2ND ORDER HIGH PASS

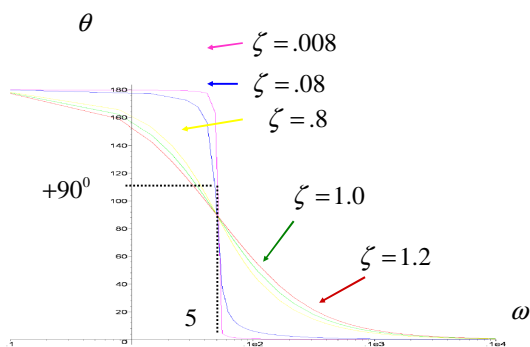
```
> with(plots):
Warning, the name changecoords has been redefined
> H1:=(1000*s^2)/(s^2+12*s+25):
> H2:=(1000*s^2)/(s^2+10*s+25):
> H3:=(1000*s^2)/(s^2+8*s+25):
> H4:=(1000*s^2)/(s^2+.8*s+25):
> H5:=(1000*s^2)/(s^2+.08*s+25):
> #High Pass,  wo = 5, Damping Ratio = 1.2, 1.0, .8, .08, .008
> #Overdamped, Critically Damped, Underdamped, Very Underdamped
> s:=I*omega:
> g1:=20*log10(abs(H1)):
> g2:=20*log10(abs(H2)):
> g3:=20*log10(abs(H3)):
> g4:=20*log10(abs(H4)):
> g5:=20*log10(abs(H5)):
> theta1:=(180/Pi)*argument(H1):
> theta2:=(180/Pi)*argument(H2):
> theta3:=(180/Pi)*argument(H3):
> theta4:=(180/Pi)*argument(H4):
> theta5:=(180/Pi)*argument(H5):
> semilogplot([g1,g2,g3,g4,g5],omega=1..50):
```



2ND ORDER HIGH PASS



2ND ORDER HIGH PASS



2ND ORDER BANDPASS

$$\text{Bandpass: } H1_{HP}(s) = \frac{1000s}{s^2 + 12s + 25}; \quad \zeta = 1.2$$

$$H2_{HP}(s) = \frac{1000s}{s^2 + 10s + 25}; \quad \zeta = 1.0$$

$$\omega_0 = 5 \quad H3_{HP}(s) = \frac{1000s}{s^2 + 8s + 25}; \quad \zeta = .8$$

$$H4_{HP}(s) = \frac{1000s}{s^2 + .8s + 25}; \quad \zeta = .08$$

$$H5_{HP}(s) = \frac{1000s}{s^2 + .08s + 25}; \quad \zeta = .008$$



2ND ORDER BANDPASS

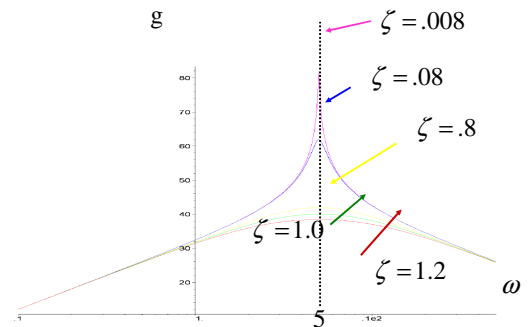
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> with(plots):
Warning, the name changecoords has been redefined
H1:=(1000*s)/(s^2+12*s+25):
H2:=(1000*s)/(s^2+10*s+25):
H3:=(1000*s)/(s^2+8*s+25):
H4:=(1000*s)/(s^2+.8*s+25):
H5:=(1000*s)/(s^2+.08*s+25):
#wo = 5, Damping Ratio = 1.2, 1.0, .8, .08, .008
#Overdamped, Critically Damped, Underdamped
#Bandpass Filter
s:=I*omega:
g1:=20*log10(abs(H1)):
g2:=20*log10(abs(H2)):
g3:=20*log10(abs(H3)):
g4:=20*log10(abs(H4)):
g5:=20*log10(abs(H5)):
theta1:=(180/Pi)*argument(H1):
theta2:=(180/Pi)*argument(H2):
theta3:=(180/Pi)*argument(H3):
theta4:=(180/Pi)*argument(H4):
theta5:=(180/Pi)*argument(H5):
semilogplot([g1,g2,g3,g4,g5],omega=.1..50):

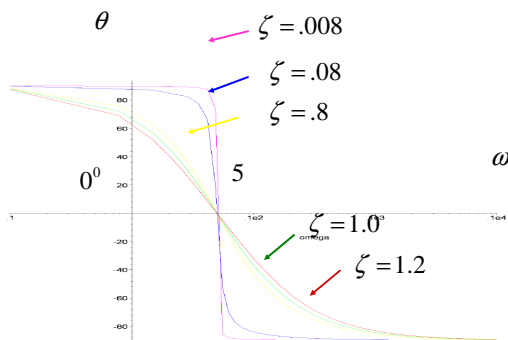
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2ND ORDER BANDPASS



2ND ORDER BANDPASS



2ND ORDER FILTERS

Always See Resonance When We Have
Complex Conjugate Poles
 $\zeta < 1 \Rightarrow$ Underdamping

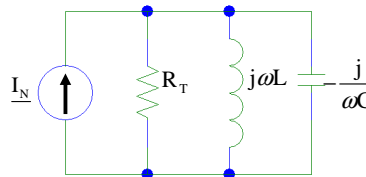
Avoid Resonance for Good Low Pass
and High Pass Filters

Use Resonance for Good Bandpass
and Bandgap Filters



PARALLEL RESONANCE

Frequency Domain



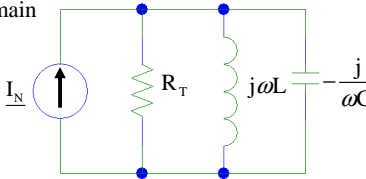
$$Y_{eq} = \frac{1}{R_T} + \frac{1}{j\omega L} + \frac{\omega C}{-j} = \frac{1}{R_T} + j\left(\omega C - \frac{1}{\omega L}\right)$$

$$= G(\omega) + jB(\omega)$$



PARALLEL RESONANCE

Frequency Domain



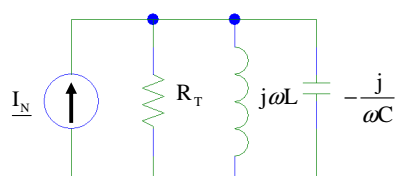
$$Y_{eq} = \frac{1}{R_T} + j\left(\omega C - \frac{1}{\omega L}\right) = G(\omega) + jB(\omega)$$

AC Susceptance = $B(\omega) \rightarrow 0$ when $\omega = \omega_0 = \sqrt{\frac{1}{LC}}$



PARALLEL RESONANCE

Frequency Domain



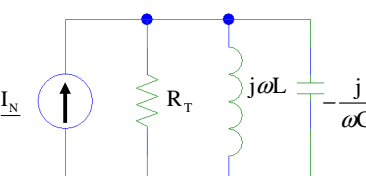
$$\omega_0 = \sqrt{\frac{1}{LC}}$$

ω_0 = Resonant Frequency
 \Rightarrow Same as for Series Resonance



PARALLEL RESONANCE

Frequency Domain

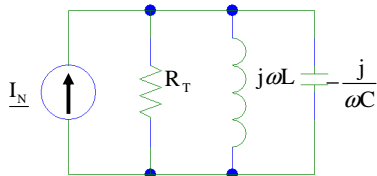


$$Y_{eq} = \frac{1}{R_T} \text{ at } \omega = \omega_0$$

$\Rightarrow Z_{eq}(\omega_0) = R_T$; Purely Resistive



PARALLEL RESONANCE



$$|Y_{eq}(\omega)| = \sqrt{G^2 + B^2}; B(\omega_0) \rightarrow 0$$

$$\Rightarrow |Y_{eq}| \text{ is a MINIMUM at } \omega = \omega_0$$

$$\Rightarrow |Z_{eq}| \text{ is a MAXIMUM at } \omega = \omega_0$$



TYPE OF RESONANCE

Parallel Resonance:

$$\Rightarrow |Z_{eq}| = \text{MAXIMUM at } \omega = \omega_0$$

Series Resonance:

$$\Rightarrow |Z_{eq}| = \text{MINIMUM at } \omega = \omega_0$$

Often the best way to determine type of resonance



PARALLEL RESONANCE

KCL: $I_L + I_C + I_R = I_N$; At Resonance: $I_L = -I_C$

$$\underline{V} = I_N Z_{eq} = I_R R_T = I_L (j\omega L) = I_C \left(\frac{1}{j\omega C} \right)$$

At $\omega = \omega_0$; $Z_{eq} = R_T$

$$\Rightarrow \frac{I_L}{I_N} = \frac{R_T}{j\omega_0 L} \Rightarrow \frac{|I_L|}{|I_N|} = \frac{R_T}{\omega_0 L}$$

$$\Rightarrow \frac{I_C}{I_N} = R_T j\omega_0 C \Rightarrow \frac{|I_C|}{|I_N|} = \omega_0 R_T C$$



PARALLEL RESONANCE

$$\text{At Resonance: } \omega_0 C R_T = \frac{R_T}{\omega_0 L}; \omega_0 = \sqrt{\frac{1}{LC}};$$

$$\Rightarrow Q_{\text{parallel}} = \frac{|I_C|}{|I_N|} = \frac{|I_L|}{|I_N|} = R_T \sqrt{\frac{C}{L}};$$

= "Current Gain" at $\omega = \omega_0$

$$\text{Note: } Q_{\text{parallel}} = \frac{1}{Q_{\text{series}}}$$



PARALLEL RESONANCE

For $Q_{\text{parallel}} \gg 1$:

Want "large" R_T , "small" L , "large" C

Just the opposite of what makes $Q_{\text{series}} \gg 1$

\Rightarrow A good Series Resonant circuit will be
a lousy Parallel Resonant circuit



SUMMARY

Series Resonance:

$$X \rightarrow 0 \text{ at } \omega = \omega_0$$

$$\omega_0 = \sqrt{\frac{1}{LC}}$$

$$Q_{\text{series}} = \frac{1}{R_T} \sqrt{\frac{L}{C}}$$

$$|Z_{\text{eq}}(\omega_0)| = \text{MINIMUM}$$

Parallel Resonance:

$$B \rightarrow 0 \text{ at } \omega = \omega_0$$

$$\omega_0 = \sqrt{\frac{1}{LC}}$$

$$Q_{\text{parallel}} = R_T \sqrt{\frac{C}{L}}$$

$$|Z_{\text{eq}}(\omega_0)| = \text{MAXIMUM}$$



NOTES ON RESONANCE

- In "real" circuits, often do not have a "pure" Series or "pure" Parallel situation:

- Inductors always have R_w
- Elements may not all be in series or parallel
- Will still have Resonance, but at a slightly different Resonant Frequency



NOTES ON RESONANCE

- In "real" circuits, often do not have a "pure" Series or "pure" Parallel situation:

- May also have Multiple Resonances in same Circuit
- Define Resonance as when X (series-like circuit) or B (parallel-like circuit) $=> 0$
- Let's do an Example

